

CBCS SCHEME

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18EC55

Fifth Semester B.E. Degree Examination, Jan./Feb. 2023

Electromagnetic Waves

Time: 3 hrs.

Max. Marks: 100

Note: Answer any FIVE full questions, choosing ONE full question from each module.

Module-1

- The three vertices of a triangle are located at $A(6, -1, 2)$, $B(-2, 3, -4)$ and $C(-3, 1, 5)$. Find (i) $R_{AB} \times R_{AC}$ (ii) Area of triangle (04 Marks)
 - Define Electric field intensity. Derive the expression for electric field intensity due to infinite line charge. (10 Marks)
 - Given the electric flux density $\bar{D} = 0.3r^2 \bar{a}_r \text{ C/m}^2$ in free space.
 - Find E at point $P(r=2, \theta=25^\circ, \phi=90^\circ)$.
 - Find total charge within the sphere $r=3$.
 - Find total electric flux leaving the sphere $r=4$. (06 Marks)

OR

- Four identical 3 nC (nano Coulomb) charges are located at $P_1(1, 1, 0)$, $P_2(-1, 1, 0)$, $P_3(-1, -1, 0)$ and $P_4(1, -1, 0)$. Find the electric field intensity \bar{E} at $P(1, 1, 1)$. (10 Marks)
 - Infinite uniform line charges of 5 nC/m lie along the (positive and negative) x and y axes in free space. Find \bar{E} at $P(0, 0, 4)$. (04 Marks)
 - Define Coulomb's law. Make use of this to find the force on Q_1 . Given that the point charges $Q_1 = 50 \mu\text{C}$ and $Q_2 = 10 \mu\text{C}$ are located at $(-1, 1, -3) \text{ m}$ and $(3, 1, 0) \text{ m}$ respectively. (06 Marks)

Module-2

- Explain Gauss law applicable to the case of infinite line charge and derive the relation used. (08 Marks)
 - Evaluate both sides of the divergence theorem for the field $\bar{D} = 2xy\bar{a}_x + x^2\bar{a}_y \text{ C/m}^2$ and the rectangular parallelepiped formed by the planes $x=0$ and 1 , $y=0$ and 2 and $z=0$ and 3 . (08 Marks)
 - Given the potential field $V = 2x^2y - 5z$ and point $P(-4, 3, 6)$. (i) Find potential V at P . (ii) Field intensity \bar{E} , (iii) Volume charge density ρ_v . (04 Marks)

OR

- Compute the numerical value for $\text{div} \bar{D}$ at the point specified below:
 $\bar{D} = (2xyz - y^2)\bar{a}_x + (x^2z - 2xy)\bar{a}_y + x^2y\bar{a}_z \text{ C/m}^2$ at $P_A(2, 3, -1)$ (04 Marks)
 - Show that Electric field is a negative gradient of potential. (08 Marks)
 - Let $E = y\bar{a}_x \text{ V/m}$ at a certain instant of time and calculate the work required to move a 3 C charge from $(1, 3, 5)$ to $(2, 0, 3)$ along the straight line segment joining
 - $(1, 3, 5)$ to $(2, 3, 5)$ to $(2, 0, 5)$ to $(2, 0, 3)$
 - $(1, 3, 5)$ to $(1, 3, 3)$ to $(1, 0, 3)$ to $(2, 0, 3)$ (08 Marks)

1 of 3

Important Note : 1. On completing your answers, compulsorily draw diagonal cross lines on the remaining blank pages.
2. Any revealing of identification, appeal to evaluator and/or equations written eg. $42+8=50$, will be treated as malpractice.

Module-3

- 5 a. Solve the Laplace's equation for the potential field in the homogenous region between the two concentric conducting spheres with radii 'a' and 'b' such that $b > a$, if potential $V = 0$ at $r = b$ and $V = V_0$ at $r = a$. Also find the capacitance between two concentric spheres.

(10 Marks)

- b. State and explain Biot-Savart law applicable to magnetic field.

(06 Marks)

- c. Calculate the value of vector current density in a rectangular coordinates at $P_A(2, 3, 4)$ if

$$\vec{H} = x^2 z \vec{a}_y - y^2 x \vec{a}_z.$$

(04 Marks)

OR

- 6 a. State and illustrate uniqueness theorem.

(08 Marks)

- b. Define Stoke's theorem. Use this theorem to evaluate both sides of the theorem for the field

$$\vec{H} = 6xy \vec{a}_x - 3y^2 \vec{a}_y \text{ A/M and the rectangular path around the region, } 2 \leq x \leq 5, -1 \leq y \leq 1$$

$z = 0$. Let the positive direction of ds be \vec{a}_z .

(12 Marks)

Module-4

- 7 a. Obtain the expression for magnetic force between differential current elements. (06 Marks)

- b. Derive the boundary conditions to apply to \vec{B} and \vec{H} at the interface between two different magnetic materials. (08 Marks)

- c. The point charge $q = 18 \text{ nC}$ has a velocity of $5 \times 10^6 \text{ m/s}$ in the direction.

$$\vec{a}_v = 0.60 \vec{a}_x + 0.75 \vec{a}_y + 0.30 \vec{a}_z$$

Calculate the magnitude of the force exerted on the charge by the field,

(i) $\vec{B} = -3 \vec{a}_x + 4 \vec{a}_y + 6 \vec{a}_z \text{ mT}$

(ii) $\vec{E} = -3 \vec{a}_x + 4 \vec{a}_y + 6 \vec{a}_z \text{ kV/m}$

(iii) \vec{B} and \vec{E} acting together

(06 Marks)

OR

- 8 a. Find the magnetization in a magnetic material, where

(i) $\mu = 1.8 \times 10^{-5} \text{ H/m}$ and $H = 120 \text{ A/m}$

(ii) $\mu_r = 22$, there are $8.3 \times 10^{28} \text{ atoms/m}^3$, and each atom has a dipole moment of $4.5 \times 10^{-27} \text{ A.m}^2$

(iii) $B = 300 \mu\text{T}$ and $\chi_m = 15$.

(06 Marks)

- b. Let permittivity be $5 \mu\text{H/m}$ in region A where $x < 0$ and $20 \mu\text{H/m}$ in region B, where $x > 0$.

If there is a surface current density $\vec{K} = 150 \vec{a}_y - 200 \vec{a}_z \text{ A/m}$ at $x = 0$, and if

$$\vec{H}_A = 300 \vec{a}_x - 400 \vec{a}_y + 500 \vec{a}_z \text{ A/m. Compute}$$

(i) $|H_{tA}|$ (ii) $|H_{nA}|$ (iii) $|H_{tB}|$ (iv) $|H_{nB}|$

(08 Marks)

- c. State and explain Faraday's law of electromagnetic induction.

(06 Marks)

Module-5

- 9 a. List and explain Maxwell's equations in point and integral form.

(08 Marks)

- b. The time domain expression for the magnetic field of a uniform plane wave travelling in free space is given by,

$$H(z,t) = \bar{a}_y 2.5 \cos(1.257 \times 10^9 t - K_0 z) \text{ mA/m.}$$

Compute

- (i) The direction of wave propagation.
 - (ii) Operating frequency
 - (iii) Phase constant.
 - (iv) The time domain expression for electric field $E(z,t)$ starting from the Maxwell's equations.
 - (v) The phasor form of both the electric and magnetic field. (10 Marks)
- c. For silver the conductivity is $\sigma = 3 \times 10^6 \text{ S/m}$. At what frequency will the depth of penetration be 1 mm. (02 Marks)

OR

- 10 a. State and explain Poynting theorem and write the equation both in point and integral form. (08 Marks)
- b. Simplify the value of K to satisfy the Maxwell's equations for region $\sigma = 0$ and $\rho_v = 0$ if $\bar{D} = 10x\bar{a}_x + 4y\bar{a}_y + kz\bar{a}_z \text{ } \mu\text{C/m}^2$ and $B = 2a_y \text{ mT}$. (06 Marks)
- c. A plane wave of 16 GHz frequency and $E = 10 \text{ V/m}$ propagates through the body of salt water having constant $\epsilon_r = 100$, $\mu_r = 1$ and $\sigma = 100 \text{ s/m}$. Determine attenuation constant, phase constant, phase velocity and intrinsic impedance and depth and penetration. (06 Marks)

Module - 1

1]

(a) i) $\vec{R}_{AB} = \vec{R}_B - \vec{R}_A = \langle -2, 3, -4 \rangle - \langle 6, -1, 2 \rangle = -8\hat{a}_x + 4\hat{a}_y - 6\hat{a}_z$

$\vec{R}_{AC} = \vec{R}_C - \vec{R}_A = \langle -3, 1, 5 \rangle - \langle 6, -1, 2 \rangle = -9\hat{a}_x + 2\hat{a}_y + 3\hat{a}_z$

$\vec{R}_{AB} \times \vec{R}_{AC} =$

\hat{a}_x	\hat{a}_y	\hat{a}_z
-8	4	-6
-9	2	3

-2M

$\vec{R}_{AB} \times \vec{R}_{AC} = 24\hat{a}_x + 78\hat{a}_y + 20\hat{a}_z$

ii) Area of triangle = $\frac{1}{2} |\vec{R}_{AB} \times \vec{R}_{AC}| =$

$= \frac{1}{2} \left[\sqrt{(24)^2 + (78)^2 + (20)^2} \right] = 42 \text{ sq unit}$

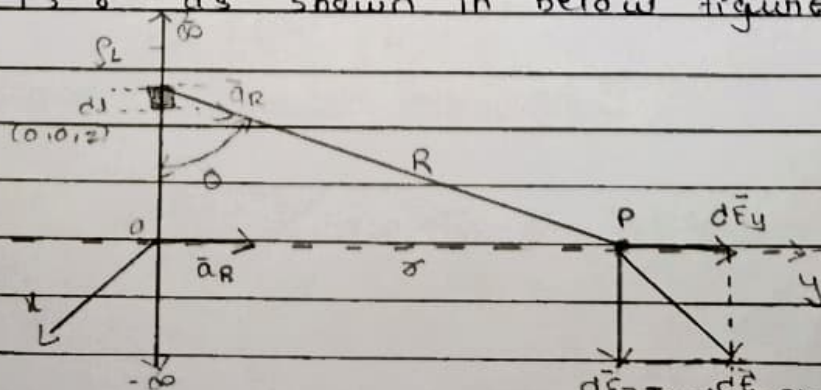
-2M

1]

(b) Electric field intensity :- The force exerted per unit charge is called electric field intensity.

$E = \frac{F}{q} \text{ V/m}$

Consider a long straight line carrying uniform line charge having density $\rho_L \text{ C/m}$. Let a point P is on y-axis at which electric field intensity is to be determined. The distance of point P from the origin is 'x' as shown in below figure



4M

Teacher's Sign.

□ (b)

$$dQ = \rho_L du = \rho_L dz \quad - (1)$$

$$\vec{R} = \vec{r}_p - \vec{r}_d = [x\vec{a}_y - z\vec{a}_z]$$

$$|\vec{R}| = \sqrt{x^2 + z^2}$$

$$\vec{a}_R = \frac{\vec{R}}{|\vec{R}|} = \frac{x\vec{a}_y - z\vec{a}_z}{\sqrt{x^2 + z^2}} \quad - (2)$$

$$d\vec{E} = \frac{dQ}{4\pi\epsilon_0 R^2} \vec{a}_R$$

$$= \frac{\rho_L dz}{4\pi\epsilon_0 [\sqrt{x^2 + z^2}]^2} \left[\frac{x\vec{a}_y - z\vec{a}_z}{\sqrt{x^2 + z^2}} \right] \quad - (3)$$

For every charge on positive z-axis there is equal charge present on negative z-axis. So z-component will cancel out each other. So, by eliminating z component

$$d\vec{E} = \frac{\rho_L dz}{4\pi\epsilon_0 (\sqrt{x^2 + z^2})^2} \frac{x\vec{a}_y}{\sqrt{x^2 + z^2}} \quad - (4)$$

$$E = \int_{-\infty}^{\infty} \frac{\rho_L}{4\pi\epsilon_0 (x^2 + z^2)^{3/2}} x dz \vec{a}_y$$

$$z = x \tan \theta \quad x = z / \tan \theta \quad dz = x \sec^2 \theta d\theta$$

for $z = -\infty$, $\theta = \tan^{-1}(-\infty) = -\pi/2$; $z = \infty$, $\theta = \tan^{-1}(\infty) = \pi/2$

$$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{-\pi/2}^{\pi/2} \frac{x^2 \sec^2 \theta d\theta}{x^3 [1 + \tan^2 \theta]^{3/2}} \vec{a}_y$$

$$E = \frac{\rho_L}{4\pi\epsilon_0} \int_{-\pi/2}^{\pi/2} \frac{\sec^2 \theta d\theta}{x \sec^3 \theta} \vec{a}_y = \frac{\rho_L}{4\pi\epsilon_0 x} \int_{-\pi/2}^{\pi/2} \cos \theta d\theta \vec{a}_y$$

$$E = \frac{\rho_L}{4\pi\epsilon_0 x} \left[\sin \theta \right]_{-\pi/2}^{\pi/2} \vec{a}_y = \frac{\rho_L}{4\pi\epsilon_0 x} [1 - (-1)] \vec{a}_y$$

$$E = \frac{\rho_L}{2\pi\epsilon_0 x} \vec{a}_y \quad \text{V/m}$$

GM

1]

(c) i) We know that electric flux density $(D) = \epsilon_0 E$

$$E = D / \epsilon_0$$

$$D = 0.3 \times 10^{-2} \hat{a}_z \text{ nC/m}^2 \quad \text{at } z = 2 \quad \underline{2M}$$

$$E = 135.2 \text{ V/m}$$

(ii) $D = \frac{Q}{4\pi r^2} \quad Q = 4 \times \pi \times r^2 \times D$ 2M

$$D = 4 \times 3.14 \times (3)^2 \times 0.3 \times (3)^2$$

$$D = 305.208 \text{ nC}$$

(iii) We know that $Q = \phi$ at $z = 4$ 2M

$$D = \frac{Q}{4\pi r^2} = Q = 4\pi r^2 \times D$$

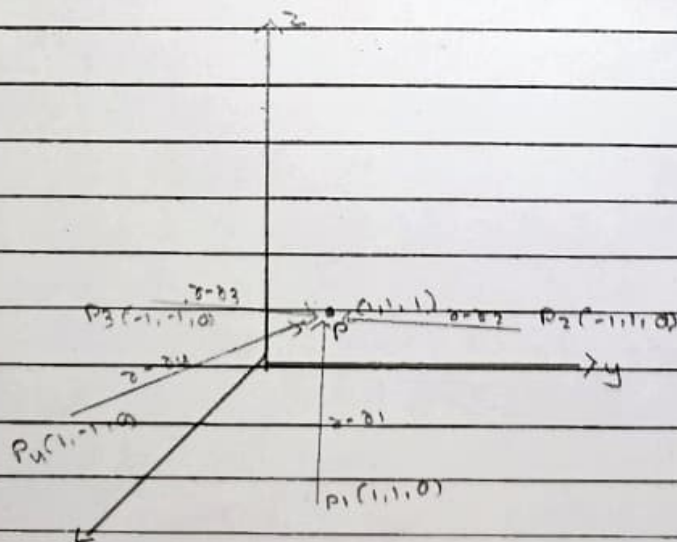
$$Q = 4 \times 3.14 \times (4)^2 \times (0.3) \times (4)^2$$

$$Q = 964.608 \text{ nC}$$

$$\phi = 965 \text{ nC}$$

2]

(a)



$$\begin{aligned} \sigma_1 &= ax + ay & \sigma_2 &= -ax + ay \\ \sigma_3 &= ax + ay + az & \sigma_4 &= -ax - ay \end{aligned}$$

KLS, VPIIT, Halyal

2] (a)

$$r - r_1 = \langle 1, 1, 1 \rangle - \langle 1, 1, 0 \rangle = \langle 0, 0, 1 \rangle = \hat{j} \quad \left. \vphantom{r - r_1} \right\} 4M$$

$$|r - r_2| = \sqrt{5}, \quad |r - r_3| = 3 \quad \text{and} \quad |r - r_4| = \sqrt{5}$$

$$E = 26.96 \left[\frac{0\hat{z} \cdot 1}{1^2} + \frac{20\hat{x} + 0\hat{z} \cdot 1}{\sqrt{5} (\sqrt{5})^2} + \frac{20\hat{x} + 20\hat{y} + 0\hat{z} \cdot 1}{3^3} + \frac{20\hat{y} + 0\hat{z} \cdot 1}{\sqrt{5} (\sqrt{5})^2} \right] \quad 4M$$

$$E = 6.82\hat{a}_x + 6.82\hat{a}_y + 32.8\hat{a}_z \text{ V/m} \quad // \quad 2M$$

2]

(b)

Electric field at uniform line charge is given by

$$E = \frac{\lambda}{2\pi\epsilon_0 r} \hat{a}_r = \frac{5 \times 10^{-9}}{2 \times 3.14 \times \epsilon_0 (4)} \cdot 4\hat{a}_z + \frac{5 \times 10^{-9}}{2 \times \pi \times \epsilon_0 (4)} \cdot 4\hat{a}_z \quad 2M$$

$$E = 45\hat{a}_z \text{ V/m} \quad 2M$$

2]

(c)

The coulomb's law states that the force between two point charges is directly proportional to the product of magnitude of charge and inversely proportional to the square of distance between them. 1M

$$F \propto \frac{Q_1 Q_2}{r^2}$$

$$F = \frac{1}{4\pi\epsilon_0} \frac{Q_1 Q_2}{r^2} \quad //$$

$$Q_1 = 5 \mu\text{C}$$

$$Q_2 = 10 \mu\text{C} \quad 5M$$

$$r_1 = \langle -1, 1, -3 \rangle$$

$$r_2 = \langle 3, 1, 0 \rangle$$

$$r = r_1 - r_2 = -4\hat{a}_x - 3\hat{a}_z$$

2] (c)

$$\vec{a}_x = \frac{\vec{a}}{|\vec{a}|} = \frac{-4ax - 3a^2}{5}$$

$$F = \frac{Q_1 Q_2}{4 \times \pi \times \epsilon_0 \times r^2} \vec{a}_x$$

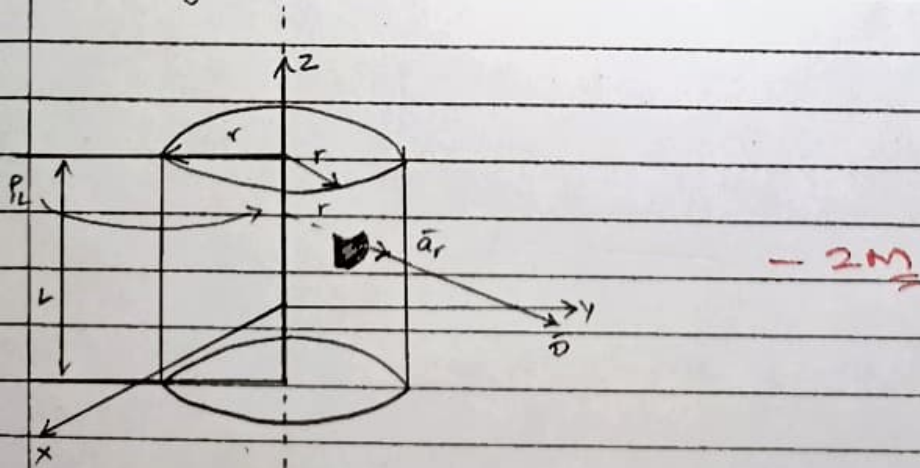
$$F = \frac{50 \times 10^{-9} \times 10 \times 10^{-9}}{4 \times 3.14 \times 8.85 \times 10^{-12} \times (5)^2 \times 5} \times (-4ax - 3a^2)$$

$$F = -0.144 a \vec{x} - 0.108 a^2 \vec{a} \text{ N.}$$

Module - 2

3]

(a) Consider an infinite line charge of density ρ_L C/m lying along z-axis from $-\infty$ to ∞ . Consider the gaussian surface as the right circular cylinder with z-axis as its axis and radius a . The length of cylinder is L .



Consider differential surface area dS as shown which is at the radial distance a from the line charge.

KLS, VDI, Halyal

3] As the line charge is along z-axis there cannot be any component of \vec{D} in z-direction

$$\text{Now } Q = \oint_S \vec{D} \cdot d\vec{S}$$

The integration is to be evaluated for side, top and bottom surface

$$Q = \oint_{\text{side}} \vec{D} \cdot d\vec{S} + \oint_{\text{top}} \vec{D} \cdot d\vec{S} + \oint_{\text{bottom}} \vec{D} \cdot d\vec{S}$$

$\vec{D} = D_r \vec{a}_r$ as has only radial component

$d\vec{S} = r d\phi dz \vec{a}_z$ normal to \vec{a}_z direction

$$\vec{D} \cdot d\vec{S} = D_r r d\phi dz$$

3M

As \vec{D} has only radial component and no z-component along \vec{a}_z and $-\vec{a}_z$ hence integrating over top and bottom surfaces is zero.

$$\oint_{\text{top}} \vec{D} \cdot d\vec{S} = \oint_{\text{bottom}} \vec{D} \cdot d\vec{S} = 0$$

$$Q = \oint_{\text{side}} \vec{D} \cdot d\vec{S} = \oint_{\text{side}} D_r r d\phi dz = \int_{z=0}^L \int_{\phi=0}^{2\pi} D_r r d\phi dz$$

$$Q = r D_r [z]_0^L [\phi]_0^{2\pi}$$

$$Q = 2\pi r D_r L$$

$$D_r = \frac{Q}{2\pi r L}$$

$$\vec{D} = D_r \vec{a}_r = \frac{Q}{2\pi r L} \vec{a}_r$$

$$Q/L = \rho_L \text{ C/m}$$

$$\vec{D} = \frac{\rho_L}{2\pi r} \vec{a}_r \text{ C/m}^2$$

$$\vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{\rho_L}{2\pi \epsilon_0 r} \vec{a}_r \text{ V/m}$$

3M

3]

(b)

Divergence theorem

$$\oint_S \vec{n} \cdot d\vec{s} = \int_{vol} \nabla \cdot \vec{D} dv$$

$$\oint \vec{D} \cdot d\vec{s} = \oint_{front} \vec{D} \cdot d\vec{s} + \oint_{back} \vec{D} \cdot d\vec{s} + \oint_{left} \vec{D} \cdot d\vec{s} + \oint_{right} \vec{D} \cdot d\vec{s}$$

$$\begin{aligned} \oint_{front} \vec{D} \cdot d\vec{s} &= \int_0^3 \int_0^2 (\vec{D})_{x=1} \cdot dy dz \hat{i} = \int_0^3 \int_0^2 2y dy dz \\ &= \int_0^3 4 dz = \underline{\underline{12}} \end{aligned}$$

$$\oint_{back} \vec{D} \cdot d\vec{s} = \int (\vec{D})_{x=0} \cdot dy dz (-\hat{i}) = \int -(D_x)_{x=0} dy dz$$

$$\begin{aligned} &= 0 \\ \oint_{left} \vec{D} \cdot d\vec{s} &= \int (\vec{D})_{y=0} \cdot dx dz (-\hat{j}) = \int -(D_y)_{y=0} dx dz \\ &= - \int_0^3 \int_0^1 x^2 dx dz = - \int_0^3 \left[\frac{x^3}{3} \right]_0^1 dz = -3 \times \frac{1}{3} = \underline{\underline{-1}} \end{aligned}$$

$$\begin{aligned} \oint_{right} \vec{D} \cdot d\vec{s} &= \int (\vec{D})_{y=2} \cdot dx dz (\hat{j}) = \int (D_y)_{y=2} dx dz \\ &= \int_0^3 \int_0^1 x^2 dx dz = \int_0^3 \left[\frac{x^3}{3} \right]_0^1 dz = 3 \times \frac{1}{3} = \underline{\underline{1}} \end{aligned}$$

~~∮~~

$$\oint \vec{D} \cdot d\vec{s} = 12 + 0 - 1 + 1 = 12 \text{ // LHS}$$

$$\nabla \cdot \vec{D} = \frac{\partial}{\partial x} D_x + \frac{\partial}{\partial y} D_y + \frac{\partial}{\partial z} D_z$$

$$\frac{\partial}{\partial x} D_x = \frac{\partial}{\partial x} (2xy) = 2y$$

$$\frac{\partial}{\partial y} D_y = \frac{\partial}{\partial y} (x^2) = 0 \quad \frac{\partial}{\partial z} D_z = 0$$

KLS, VOIT, Halyal

3] (b)

$$\int_0^3 \int_0^2 \int_0^1 \nabla \cdot \vec{D} \, dV$$

$$\int_0^3 \int_0^2 \int_0^1 2y \, dx \, dy \, dz$$

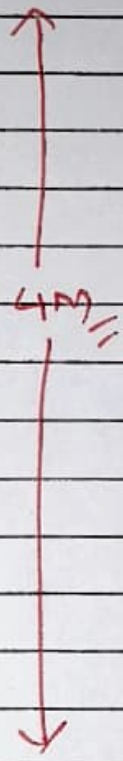
$$\int_0^3 \int_0^2 2y \, dy \, dz$$

$$\int_0^3 \left[\frac{2y^2}{2} \right]_0^2 dz$$

$$\int_0^3 4 \, dz = 12 \text{ // } \text{Ans}$$

$$\iiint \nabla \cdot \vec{D} \, dV = 12 = \text{RHS //}$$

LHS = RHS Hence divergence theorem is verified on the both side of integral



3]

(r)

$$V = 2x^2y - 5z, \text{ @ } P(4, 3, 6)$$

$$V = 2[-4]^2 \times 3 - 5 \times 6 = 66 \text{ V}$$

$$\vec{E} = -\nabla V = - \left[\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right]$$

2M //

$$= - [4xy \hat{a}_x + 2x^2 \hat{a}_y + -5 \hat{a}_z] \quad \text{--- (1)}$$

$$\text{@ } P, \quad \vec{E} = 48 \hat{a}_x - 32 \hat{a}_y + 5 \hat{a}_z \text{ V/m}$$

$$D \text{ @ } P = \vec{E} \text{ @ } P \times \epsilon_0 = 0.425 \hat{a}_x - 0.2833 \hat{a}_y + 0.0442 \hat{a}_z \text{ nC/m}^2$$

$$\rho_v = \nabla \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$

2M //

$$= 60[-4y + 0 + 0] = -4 \epsilon_0 y \text{ C/m}^3 = -35.44 \text{ pC/m}^3$$

4]

$$(a) \quad \vec{D} = (2xyz - y^2) \hat{a}_x + (x^2z - 2xy) \hat{a}_y + x^2y \hat{a}_z \text{ C/m}^2$$

$$\text{@ point } A = (2, 3, -1)$$

2M

$$\nabla \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$

$$\nabla \cdot \vec{D} = \frac{\partial (2xyz - y^2)}{\partial x} + \frac{\partial (x^2z - 2xy)}{\partial y} + \frac{\partial (x^2y)}{\partial z}$$

$$\nabla \cdot \vec{D} = 2yz + -2x$$

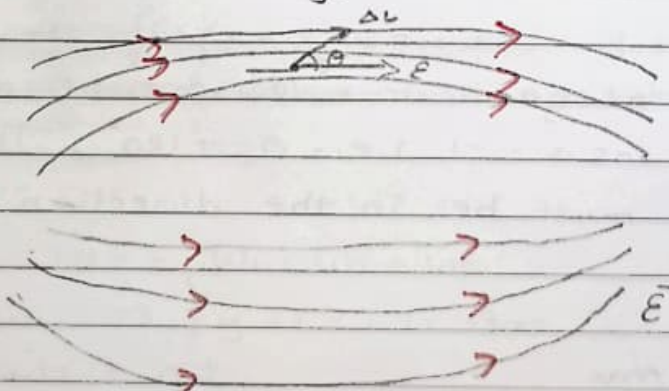
$$\nabla \cdot \vec{D} = 2 \times 3 \times (-1) + -2(2)$$

$$\nabla \cdot \vec{D} = -6 + 4 = -10$$

2M

4]

(b) Consider a \vec{E} due to particular charge distribution in space. The electric field \vec{E} and potential V is changing from point to point in space. Consider a vector incremental length $\Delta \vec{l}$ making an angle θ with respect to the direction of \vec{E} , as shown in below fig.



4M

To, find incremental potential we use,

$$\Delta V = -\vec{E} \cdot \Delta \vec{l} \quad - (1)$$

$$\Delta \vec{l} = \Delta L \hat{a}_l \quad - (2)$$

Topic :

KLS, VBIT, HANMANGAL, 2019

4] (b)

where \hat{a}_L = Unit vector in the direction of ΔL

$$\vec{E} \cdot \Delta \vec{L} = (E_L \hat{a}_L) \cdot (\Delta L \hat{a}_L)$$

$$\vec{E} \cdot \Delta \vec{L} = E_L \Delta L$$

$$\Delta V = -E_L \Delta L$$

where ;

 E_L = Component of \vec{E} in the direction of \hat{a}_L In other words dot product is expressed in terms of $\cos \theta$ as

$$\Delta V = -E \Delta L \cos \theta$$

$$\frac{\Delta V}{\Delta L} = -E \cos \theta$$

To find ΔV at a point, take limit $\Delta L \rightarrow 0$

$$\therefore \lim_{\Delta L \rightarrow 0} \frac{\Delta V}{\Delta L} = -E \cos \theta$$

$$\text{But } \lim_{\Delta L \rightarrow 0} \frac{\Delta V}{\Delta L} = \frac{dV}{dL} = \text{Potential gradient}$$

The potential gradient $\frac{dV}{dL}$ can be maximum only when $\cos \theta = -1$ i.e., $\theta = +180^\circ$. This indicates that ΔL must be in the direction opposite to \vec{E}

$$\therefore \left. \frac{dV}{dL} \right|_{\text{max}} = E$$

$$E = - \left. \frac{dV}{dL} \right|_{\text{max}} \hat{a}_n$$

4] (b)
 cont: The max value of rate of change of potential with distance (dv/dL) is called gradient of V .

The mathematical operation on V by which $-\vec{E}$ is ~~obta~~ obtained is called gradient and denoted as.

$$\text{Gradient of } V = \text{grad } V = \nabla V$$

$$\nabla V = \text{grad } V = -\vec{E} \text{ V/m}$$

$$\boxed{\vec{E} = -\nabla V = -(\text{grad } V)}$$

4]

(a) (i) $W = -q \int \vec{E} \cdot d\vec{L}$

$$W = W_1 + W_2 + W_3$$

$$W_1 = -3 \int_0^9 4ax + 0ay + 0az \, dx = -9j$$

$$W_2 = -3 \int_0^5 (1ax + 1ay + 0az) \, dy = 0J$$

$$W_3 = -3 \int_0^2 (4ax + 0ay + 0az) \, dz = 0J$$

$$W = -9j$$

(ii) $W = W_1 + W_2 + W_3$

$$W_1 = -3 \int_0^1 y \, dx = -3x = 0J$$

$$W_2 = 0J$$

$$W_3 = 0J$$

$$W = 0 + 0 + 0 = 0J$$

KLS, VOLD, Haliya

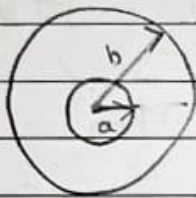
Module - 3

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5]

Q.1) The concentric sphere conductors are shown in the below figure

At $r=b$, $V=0$, hence the outer sphere is shown at zero potential.



According to Laplace's equation

$$\nabla^2 V = 0 \quad \frac{1}{r^2} \frac{\partial}{\partial r} \left[r^2 \frac{\partial V}{\partial r} \right] = 0 \quad \text{i.e.,}$$

$$\frac{\partial}{\partial r} \left[r^2 \frac{\partial V}{\partial r} \right] = 0 \quad \text{as } V \text{ is function of } r \text{ only.}$$

Integrate, $r^2 \frac{\partial V}{\partial r} = \int 0 + C_1 = C_1 \Rightarrow \frac{\partial V}{\partial r} = \frac{C_1}{r^2} = C_1 r^{-2}$ (1)

Integrate $V = \int C_1 r^{-2} dr + C_2 = \frac{C_1 r^{-1}}{-1} + C_2$ (2)

$$V = -\frac{C_1}{r} + C_2$$

Use the boundary conditions

$$V=0 \text{ @ } r=b \text{ and } V=V_0 \text{ at } r=a$$

$$0 = -\frac{C_1}{b} + C_2 \text{ and } V_0 = -\frac{C_1}{a} + C_2$$

KLS VIDYA HALLIYAL

Subtracting the two equations

$$-V_0 = \frac{-C_1}{b} - \left[\frac{-C_1}{a} \right] \text{ i.e., } -V_0 = C_1 \left[\frac{1}{a} - \frac{1}{b} \right]$$

$$\therefore C_1 = \frac{-V_0}{\left[\frac{1}{a} - \frac{1}{b} \right]} = \frac{V_0}{\left[\frac{1}{b} - \frac{1}{a} \right]} \text{ and } C_2 = \frac{C_1}{b} = \frac{V_0}{b \left[\frac{1}{b} - \frac{1}{a} \right]}$$

$$V = - \frac{V_0}{\left[\frac{1}{b} - \frac{1}{a} \right]} + \frac{V_0}{b \left[\frac{1}{b} - \frac{1}{a} \right]}$$

This is the potential field in the region between the two spheres

$$\vec{E} = -\nabla V = - \frac{\partial V}{\partial r} \hat{a}_r = - \frac{\partial}{\partial r} \left[\frac{-V_0}{\left[\frac{1}{b} - \frac{1}{a} \right]} \right] \hat{a}_r$$

$$\vec{E} = \frac{V_0}{\left[\frac{1}{b} - \frac{1}{a} \right]} \hat{a}_r \text{ V/m}$$

$$\vec{D} = \epsilon \vec{E} = \frac{-\epsilon V_0}{\left[\frac{1}{b} - \frac{1}{a} \right]} \hat{a}_r = \frac{\epsilon V_0}{\left[\frac{1}{a} - \frac{1}{b} \right]} \hat{a}_r \text{ C/m}^2$$

KLS, VDIIT, Hally...

As per the boundary conditions between conductor and dielectric, the \vec{D} is always normal to the surface hence \vec{D}_n .

$$\oint_S \vec{D}_n = \oint_S \vec{D} = \frac{\epsilon V_0}{\left[\frac{1}{a} - \frac{1}{b}\right] r^2} \quad \text{C/m}^2$$

Q = Total charge on surface of sphere of radius r

$$Q = \frac{\epsilon V_0}{\left[\frac{1}{a} - \frac{1}{b}\right] r^2} \times \text{surface area of sphere of radius } r$$

$$Q = \frac{\epsilon V_0}{\left[\frac{1}{a} - \frac{1}{b}\right] r^2} \times 4\pi r^2$$

$$Q = \frac{4\pi \epsilon V_0 r}{\left[\frac{1}{a} - \frac{1}{b}\right]}$$

$C = Q/V$ where V = Potential between two spheres = V_0

$$C = \frac{Q}{V_0} = \frac{4\pi \epsilon V_0 r}{\left[\frac{1}{a} - \frac{1}{b}\right] V_0}$$

$$C = \frac{4\pi \epsilon r}{\left[\frac{1}{a} - \frac{1}{b}\right]} \quad \text{F}$$

5]

(b) The magnetic field intensity dH produced at a point P due to differential element Idl is directly proportional to current I and differential length dl and sine of the angle between the element and the line joining point P to the element, and inversely proportional to the square of the distance R between point P and the element.

$$d\vec{H} \propto \frac{I dl \sin\theta}{R^2}$$

$$d\vec{H} = \frac{k I dl \sin\theta}{R^2}$$

k - Constant of proportionality.

$$k = \frac{1}{4\pi}$$

$$d\vec{H} = \frac{I dl \sin\theta}{4\pi R^2}$$

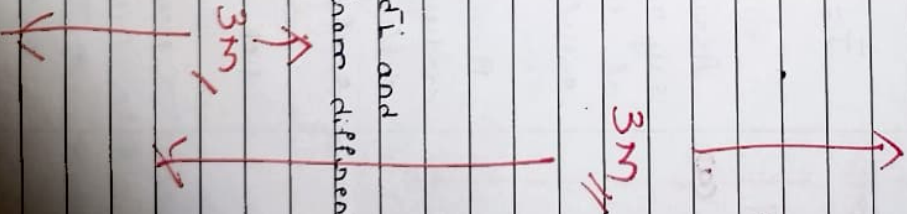
dl - magnitude of vector length dl and \vec{a}_r - Unit vector in the direction from differential current element to point P

From rule of cross product,

$$d\vec{l} \times \vec{a}_r = dl |\vec{a}_r| \sin\theta = dl \sin\theta$$

$$d\vec{H} = \frac{I d\vec{l} \times \vec{a}_r}{4\pi R^2} \quad \text{A/m}$$

$$d\vec{H} = \frac{I d\vec{l} \times \vec{R}}{4\pi R^3} \quad \text{A/m}$$



5]

(c)

Given :

$$\vec{H} = x^2 \vec{a}_x - y^2 \vec{a}_y + z^2 \vec{a}_z$$

$$\vec{J} = \nabla \times \vec{H} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & x^2 & -y^2 \end{vmatrix}$$

$$2xy \vec{a}_x + 2yz \vec{a}_y - 2xz \vec{a}_z$$

$$\vec{J} = -16x \vec{a}_x + 9ay \vec{a}_y + 16az \vec{a}_z \quad \text{A/m}^2$$

2M //

6]

(a)

Assume the Laplace's equation has two solutions say V_1 and V_2 , both are function of the coordinates of the system used. These solutions must be satisfying Laplace equation.

$$\nabla^2 V_1 = 0 \quad \text{and} \quad \nabla^2 V_2 = 0 \quad \text{--- (1)}$$

Both the solutions must satisfy the boundary conditions as well. At boundary the potentials at different points are same due to equipotential surface then,

$$V_1 = V_2 \quad \text{--- (2)}$$

Let the difference between the two solutions is V_d .

$$V_d = V_2 - V_1 \quad \text{--- (3)}$$

Using Laplace's equation for the difference V_d .

$$\nabla^2 V_d = \nabla^2 (V_2 - V_1) = 0 \quad \text{--- (4)}$$

$$\therefore \nabla^2 V_2 - \nabla^2 V_1 = 0 \quad \text{--- (5)}$$

on the boundary $V_d = 0$ from the equation (2) and (3)

$$\oint_C \vec{H} \cdot d\vec{l} = \int_S (\nabla \times \vec{H}) \cdot d\vec{s}$$

→ 20M

The line integral of a vector \vec{H} around a closed path L is equal to the integral of curl of \vec{H} over the open surface S enclosed by the closed

path L

(b)

Q

$$|\vec{v}_1 - \vec{v}_2|$$

$$v_2 - v_1 = 0$$

$$v_2 = v_2 - v_1$$

$$|\nabla v_1|^2 = 0 \text{ i.e., } \nabla v_1 = 0 \quad (12)$$

$$\therefore \int_{vol} |\nabla v_1|^2 dv = 0 \text{ as } \nabla v_1 \text{ is vector} \quad (11)$$

$$\therefore \int_{vol} \nabla v_1 - \nabla v_2 = 0 \quad (10)$$

But $v_2 = 0$ on boundary

$$\int_{vol} \nabla v_1 \cdot \nabla v_2 = \int_S \nabla v_1 \cdot \nabla v_2 \cdot d\vec{s} \quad (9)$$

$$\nabla \cdot (v_1 \nabla v_2) = \nabla v_1 \cdot \nabla v_2 + v_1 \nabla^2 v_2 \quad (8)$$

Using eq. (8)

$$\nabla \cdot (v_1 \nabla v_2) = \nabla v_1 \cdot \nabla v_2 + v_1 \nabla^2 v_2 + v_2 \nabla^2 v_1 \quad (7)$$

$$\nabla \cdot (v_1 \nabla v_2) = \nabla v_1 \cdot \nabla v_2 + v_1 \nabla^2 v_2 + v_2 \nabla^2 v_1$$

Now use this for $\nabla \cdot (v_1 \nabla v_2)$ with $v_1 = v_2$ and $\nabla v_2 = v_1$

$$\nabla \cdot (v_1 \nabla v_1) = \nabla v_1 \cdot \nabla v_1 + v_1 \nabla^2 v_1$$

Let $\vec{A} = v_1 \nabla v_1$ and from vector algebra

$$\int_{vol} \nabla \cdot \vec{A} dv = \int_S \vec{A} \cdot d\vec{s} \quad (6)$$

Now the divergence theorem states that,

(a)

Q

KLS, VBIT, Halkya

Q] (b)

According to Stoke's theorem

$$\oint_L \vec{H} \cdot d\vec{l} = \int_S (\nabla \times \vec{H}) \cdot d\vec{S}$$

$$\oint \vec{H} \cdot d\vec{l} = \int_{ab} + \int_{bc} + \int_{cd} + \int_{da} \vec{H} \cdot d\vec{l}$$

$$\int_{ab} \vec{H} \cdot d\vec{l} = \int_{x=2}^5 (6xy \vec{a}_x - 3y^2 \vec{a}_y) \cdot dx \vec{a}_x$$

$$= \int_{x=2}^5 6xy \, dx = 6y \left[\frac{x^2}{2} \right]_2^5 = \frac{6y}{2} [25 - 4] = 63y$$

5M

Now $y = -1$ for path ab, $\int_{ab} \vec{H} \cdot d\vec{l} = 63(-1) = -63$

$$\text{Similarly } \int_{bc} \vec{H} \cdot d\vec{l} = \int_{y=-1}^1 -3y^2 \, dy = -\frac{3y^3}{3} = -[y^3]_{-1}^1$$

$$= -[1 - (-1)] = -2$$

$$\int_{cd} \vec{H} \cdot d\vec{l} = \int_{x=5}^2 6xy \, dx = 6 \left[\frac{x^2}{2} \right]_5^2 (y) = \frac{6y}{2} [4 - 25] = -63y$$

But $y = 1$ for path cd hence $\int_{cd} \vec{H} \cdot d\vec{l} = -63$

$$\int_{da} \vec{H} \cdot d\vec{l} = \int_{y=1}^{-1} -3y^2 \, dy = -[y^3]_{1}^{-1} = -[(-1)^3 - (1)^3] = -[-1 + 1]$$

$$= +2$$

$$\therefore \oint \vec{H} \cdot d\vec{l} = -63 - 2 - 63 + 2 = -126 \text{ A}$$

6) (b) Now evaluate right hand side

$$\nabla \times \vec{H} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 6xy & -3y^2 & 0 \end{vmatrix}$$

$$= \vec{a}_x [0-0] + \vec{a}_y [0-0] + \vec{a}_z [0-6x] = -6x \vec{a}_z$$

$$\therefore \int_S (\nabla \times \vec{H}) \cdot d\vec{s} = \int_S (-6x \vec{a}_z) \cdot (dx dy \vec{a}_z)$$

$$d\vec{s} = dx dy \vec{a}_z \text{ normal to direction } \vec{a}_z$$

$$\therefore \int_S (\nabla \times \vec{H}) \cdot d\vec{s} = \int_{y=-1}^5 \int_{x=2}^5 -6x dx dy = -6 \left[\frac{x^2}{2} \right]_2^5 \left[y \right]_{-1}^5$$

$$= -\frac{6}{2} [25-4] [1-(-1)] = -3 \times 21 \times 2 = -126 \text{ A}$$

Thus both the side are same, hence Stokes's theorem is verified.

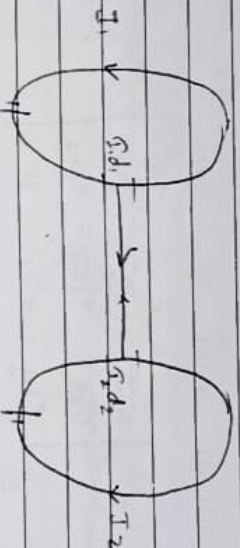
Module - 4

7)

Let us now consider two current elements $I_1 d\vec{l}_1$ and $I_2 d\vec{l}_2$ as shown in below figure. Note that the directions of I_1 and I_2 are same.

Res: VYOMIT / HATIRYADA

-1 (a)



From the equation of force the force extended on differential current element is given by

$$d(\vec{F}_1) = I_1 d\vec{l}_1 \times d\vec{B}_2 \quad - (1)$$

According to Biot - Savart's law, the magnetic field produced by current element $I_2 dl_2$ is given by for free space

$$d\vec{B}_2 = \mu_0 I_2 dl_2 = \mu_0 \left[\frac{I_2 dl_2 \times \vec{r}_{21}}{4\pi R_{21}^2} \right] \quad - (2)$$

Substituting value of $d\vec{B}_2$ in eq (1) we can write

$$d(\vec{F}_1) = \mu_0 \frac{I_1 d\vec{l}_1 \times (I_2 dl_2 \times \vec{r}_{21})}{4\pi R_{21}^2} \quad - (3)$$

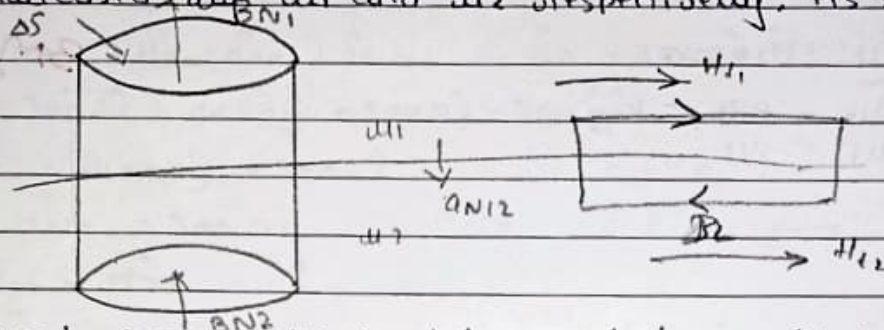
$$\vec{F}_1 = \frac{\mu_0 I_1 I_2}{4\pi} \int_{L_1} \int_{L_2} \frac{d\vec{l}_1 \times (d\vec{l}_2 \times \vec{r}_{21})}{R_{21}^2} \quad - (4)$$

Exactly following same steps, we can calculate calculate the force \vec{F}_2 extended on the current element 2.

$$\vec{F}_2 = \frac{\mu_0 I_2 I_1}{4\pi} \int_{L_2} \int_{L_1} \frac{d\vec{l}_2 \times (d\vec{l}_1 \times \vec{r}_{12})}{R_{12}^2} \quad - (5)$$

KLS, VOIF, Halkyal

7] (b) Let us consider boundary between two isotropic media 1 and 2 characterised by μ_1 and μ_2 respectively. As shown in below fig.



Normal components is determined by applying gauss law to the pill box and allowing $\Delta h \rightarrow 0$

$$\oint \vec{B} \cdot d\vec{S} = B_{1n} \Delta S - B_{2n} \Delta S = 0$$

$$\oint \vec{B} \cdot d\vec{S} = B_{1n} \Delta S - B_{2n} \Delta S = 0$$

$$B_{1n} = B_{2n}$$

$$\mu_1 H_{1n} = \mu_2 H_{2n} \Rightarrow H_{2n} = \frac{\mu_1}{\mu_2} H_{1n}$$

To determine tangential component let us apply Ampere's circuit law about small closed path abcd

$$\oint \vec{H} \cdot d\vec{l} = I$$

$$(H_{1t} - H_{2t}) \Delta L = K \Delta L$$

$$H_{1t} - H_{2t} = K$$

$$(\vec{H}_1 - \vec{H}_2) \times \vec{a}_{n12} = \vec{k}$$

An equivalent formula in terms of the vector tangential components

$$\vec{H}_{1t} - \vec{H}_{2t} = \hat{a}_{n12} \times \vec{k}$$

For tangential \vec{B} we have

$$\frac{B_{1t}}{\mu_1} - \frac{B_{2t}}{\mu_2} = k$$

Tangential component of magnetisation can be obtained as

$$H_{1t} - H_{2t} = k$$

$$M_{2t} = \frac{\chi_{m2}}{\chi_{m1}} M_{1t} - \frac{k}{\chi_{m1}}$$

KLS, VOTI, HALAYAL

7] (b) If boundary is free of current on the media are not conductors.

$$\vec{H}_{1t} - \vec{H}_{2t} = \vec{J}$$

$$\frac{\vec{B}_{1t}}{\mu_1} - \frac{\vec{B}_{2t}}{\mu_2} = \vec{K}_{//}$$

3M //

7]

(c) (i) $\vec{F}_m = Q(\vec{v} \times \vec{B})$

$$\vec{v} \times \vec{B} = 5 \times 10^3 \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0.6 & 0.7 & 0.3 \\ -3 & 4 & 6 \end{vmatrix}$$

$$\vec{v} \times \vec{B} = (3.3 \hat{a}_x - 4.5 \hat{a}_y + 4.05 \hat{a}_z) 5 \times 10^3$$

$$\vec{F}_m = Q \vec{v} \times \vec{B} = 8 \times 10^{-9} \times 5 \times 10^3 (3.3 \hat{a}_x - 4.5 \hat{a}_y + 4.05 \hat{a}_z)$$

$$|\vec{F}_m| = 660 \mu N$$

(ii) $\vec{F}_e = Q \vec{E}$

$$\vec{F}_e = 8 \mu (-3, 4, 6) = 140.6 \mu N$$

(iii) $\vec{F} = Q \vec{E} + Q \vec{v} \times \vec{B}$

$$\vec{F} = 18 \mu (-3, 4, 6) + 18 \mu \times 5 (-3.3, -4.5, 4.05)$$

$$\vec{F} = 18 \mu (-13.5, -18.5, 29.25)$$

$$|\vec{F}| = 668.7 \mu N$$

- 3M //

8]

(a) (i) $\mu = \gamma \mu_0 H$ $\gamma \mu_0 = \frac{\mu}{\mu_0} - 1$ $\mu = \mu_0 \mu_r \rightarrow \mu_r = \frac{\mu}{\mu_0}$

$$\mu = \left[\frac{\mu}{\mu_0} - 1 \right] H$$

$$\mu = 1599 \text{ A/m}$$

2M //

(ii) $\mu = \lim_{\Delta v \rightarrow 0} \frac{\sum \vec{M}_k}{\Delta v}$

$$\mu = 8.3 \times 10^{29} \times 4.5 \times 10^{-27} = 3734 \text{ A/m}$$

2M //

(iii) $B = 300 \mu T$, $\gamma \mu_0 = 15$ $\mu_0 = 1.257 \times 10^{-6}$

$$\mu = \gamma \mu_0 H$$

$$\mu = \gamma \mu_0 \frac{B}{\mu_0 \mu_r} \Rightarrow 16 \times \frac{300 \mu}{4 \pi \times 10^{-7} \times 16} = 224 \text{ A/m}$$

2M //

BLS ; VOLT, HALLWAY

Q]

(1)

$$\vec{H}_{1a} = \vec{H}_A - \vec{H}_{N1}$$

$$\vec{H}_{1a} = \vec{H}_A - (\vec{H}_A \cdot \hat{a}_{n1}) \hat{a}_{n1} = \vec{H}_A - 300 \hat{a}_x$$

$$\vec{H}_{1a} = 300 \hat{a}_x - 400 \hat{a}_y + 500 \hat{a}_z - 300 \hat{a}_x \quad \#$$

$$\vec{H}_{1a} = -400 \hat{a}_y + 500 \hat{a}_z \quad \vec{H}_{1a} = 640 \text{ A/m}$$

$$\vec{H}_{N1} = 300 \hat{a}_x$$

$$H_{N1} = 300 \text{ A/m}$$

$$\vec{H}_{1t} = \vec{H}_{2t} = \hat{a}_{n12} \Delta K$$

$$\vec{H}_{1t} - \vec{H}_{2t} = \hat{a}_{n12} \times \vec{K}$$

$$\vec{H}_{2t} = -\hat{a}_{n12} \times \vec{K} + \vec{H}_{1t}$$

$$\vec{H}_{2t} = -150 \hat{a}_z - 200 \hat{a}_y + (-400 \hat{a}_y + 500 \hat{a}_z) = -600 \hat{a}_y + 350 \hat{a}_z$$

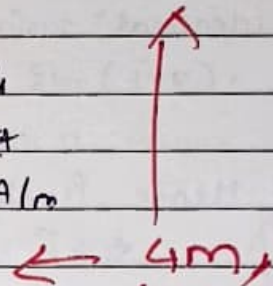
$$\vec{H}_{2t} = 695 \text{ A/m}$$

$$\frac{H_{NB}}{\mu_0} = \frac{J_2}{\mu_0}$$

$$H_{NB} = J_2$$

$$\frac{300 \hat{a}_x}{\mu_0} = \frac{20}{\mu_0}$$

$$H_{NB} = 75 \hat{a}_x \text{ A/m}$$



Q]

(1)

The EMF induced in a closed path is proportional to the rate of change of magnetic flux enclosed by the closed path.

$$e = -N \frac{d\phi}{dt} \text{ volts}$$

$N \rightarrow$ no. of turns in the circuit $e \rightarrow$ induced EMF

$$e_{\text{ind}} = \oint \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

$$\Rightarrow \oint_S (\nabla \times \vec{E}) \cdot d\vec{S} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S}$$

3m,

KL'S VIDYA HALLWAY

8]

(1) Assuming that both the surface integral taken over identical surfaces.

$$(\nabla \times \vec{E}) \cdot d\vec{s} = -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

Hence finally

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

} 3M //

Module - 5

9]

(a)

Point form

Integral form

$$\nabla \cdot \vec{D} = 0$$

$$\nabla \times \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

} (2+2)
4M

$$\oint \vec{D} \cdot d\vec{s} = 0$$

$$\oint \vec{B} \cdot d\vec{s} = 0$$

$$\oint \vec{E} \cdot d\vec{l} = -\int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

$$\oint \vec{H} \cdot d\vec{l} = \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$$

} (2+2)
4M

Explanation carrier 2M

9]

(10)

$$\delta = \frac{1}{\sqrt{\pi f \mu_0}}$$

- 2M

$$\delta = \frac{1}{\sqrt{\pi f (\mu_0 + \mu_0) \sigma}}$$

- 2M

$$1 \times 10^3 \delta = \frac{1}{\sqrt{\pi \times f \times 1 \times 4 \times \pi \times 10^{-7} \times 3 \times 10^6}}$$

- 2M

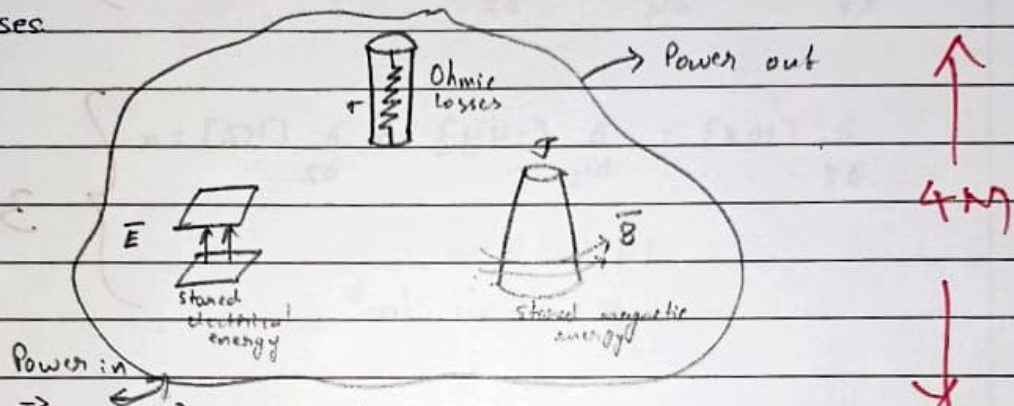
$$f = 84.4 \text{ kHz}$$

KLS, VOIT, HARRY

10]

(a)

Theorem states that the net power flowing out of the given volume V is equal to the time rate of decrease in the energy stored within V minus the ohmic losses.



As \vec{E} and \vec{H} are both vectors, to get power density we may carry out either dot product or cross product. As power flows in certain direction, it is a vector quantity so we use the cross product as the output of dot product is scalar.

The power density is given by

$$\vec{P} = \vec{E} \times \vec{H}$$

where \vec{P} is called Poynting vector.

Poynting theorem in point form

$$-\nabla \cdot \vec{P} = \sigma E^2 + \frac{1}{2} \frac{\partial}{\partial t} [\mu H^2 - \epsilon E^2]$$

Poynting theorem in integral form

$$-\oint_S \vec{P} \cdot d\vec{S} = \int_V \sigma E^2 dV + \frac{\partial}{\partial t} \int_V \frac{1}{2} [\mu H^2 + \epsilon E^2] dV$$

KLS V.D.I.T., HALIYAL

10]

(b) $\nabla \cdot \vec{D} = \rho_v = 0$

$$\frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} = 0$$

} 3M

$$\frac{\partial [10x]}{\partial x} + \frac{\partial [-4y]}{\partial y} + \frac{\partial [kz]}{\partial z} = 0$$

$$10 - 4 + k = 0$$

$$k = -6 \text{ uC/m}^3$$

} 3M

9]

(b) The wave propagates along +z direction -

$f = 200 \text{ MHz}$

- 2M

Phase constant = 4.19 rad/sec

- 2M

$E(z,t) = a_x 0.94 \cos(1.257 \times 10^9 t - 4.19z) \text{ V/m}$

- 2M

$E_s(z) = a_x 0.94 e^{-j4.19z} \text{ V/m}$

- 2M

$H_s(z) = a_y 2.5 e^{-j4.19z} \text{ mA/m}$

- 2M

[10] (c) $\frac{\sigma}{\omega\epsilon} > 1$ hence it is a good conductor

$\alpha = \beta = \sqrt{\frac{\mu_0 \omega \sigma}{2}} = 2513$

$\eta = \sqrt{\frac{10\pi \times 10^{-8}}{0}} \times 145 = 35.5 \text{ } \Omega$

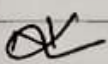
2M

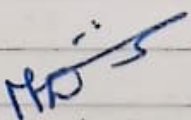
$v = \frac{c}{\beta} = 4 \times 10^7 \text{ m/s}$

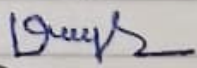
$\delta = \frac{1}{\sqrt{\pi f \sigma \mu_0}} = 2513$

} 4M

Scheme and solution prepared by Prof. Nikhil K


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